

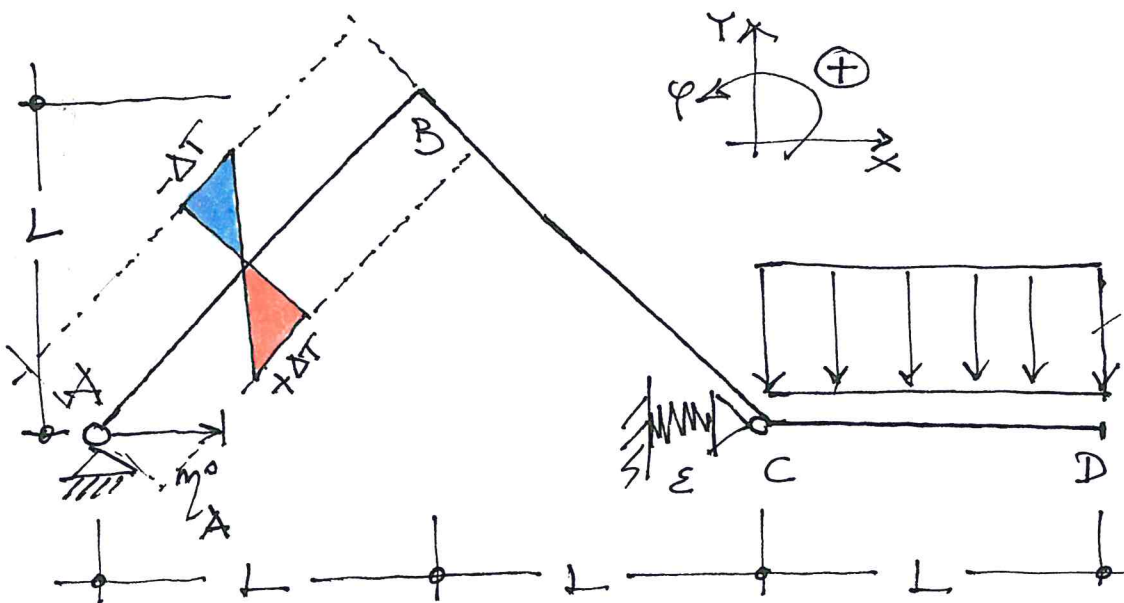
ESAMI di MECCANICA delle STRUTTURE - L17
 Corso P. FUSCHI - A.A. 2016-17 - prova scritta 28.06.17

①
 P. FUSCHI
 A. PISANO

SOLUZIONE

Quesito n. 1

RISOLVERE LA STRUTTURA UNA VOLTA IPERSTATICA RIPORTATA
 IN FIGURA TRACCIANDO IL DIAGRAMMA DEI MOMENTI



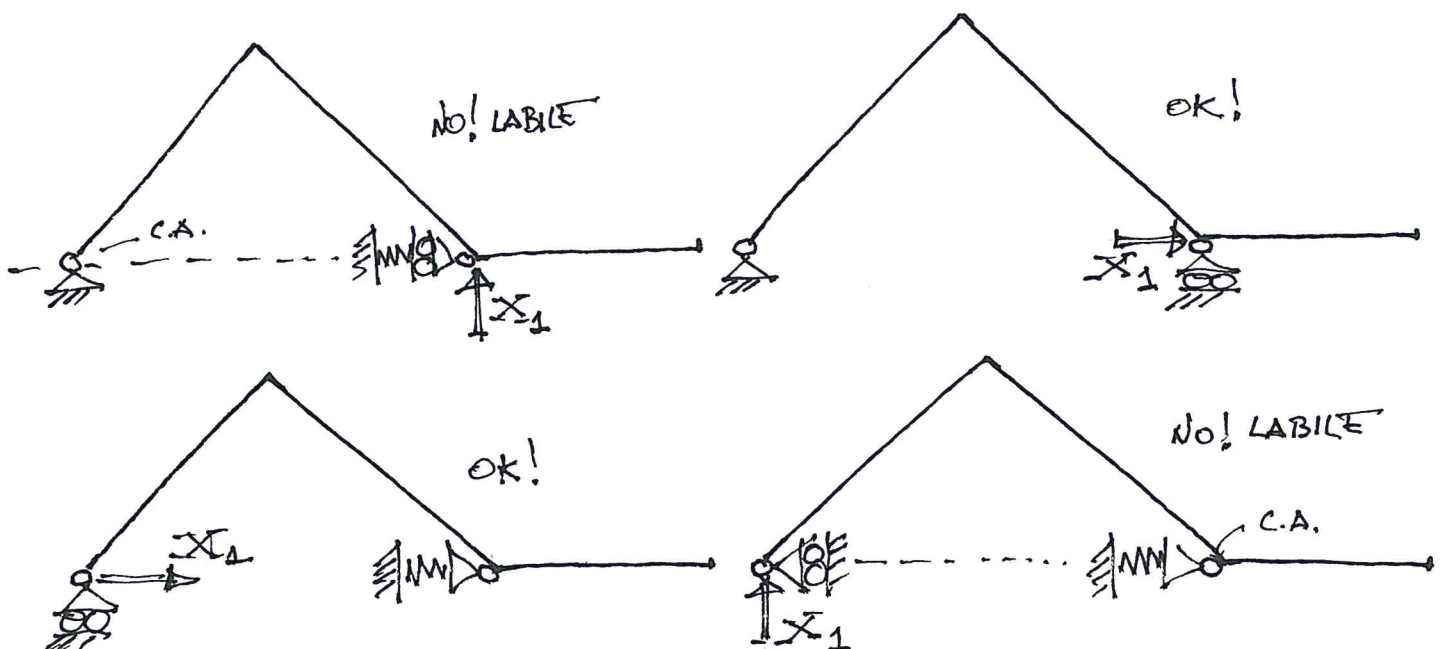
Posizioni:

$$|\varphi_A^0| = \frac{qL^4\sqrt{2}}{4EI}$$

$$|\varepsilon| = \frac{L^3\sqrt{2}}{3EI}$$

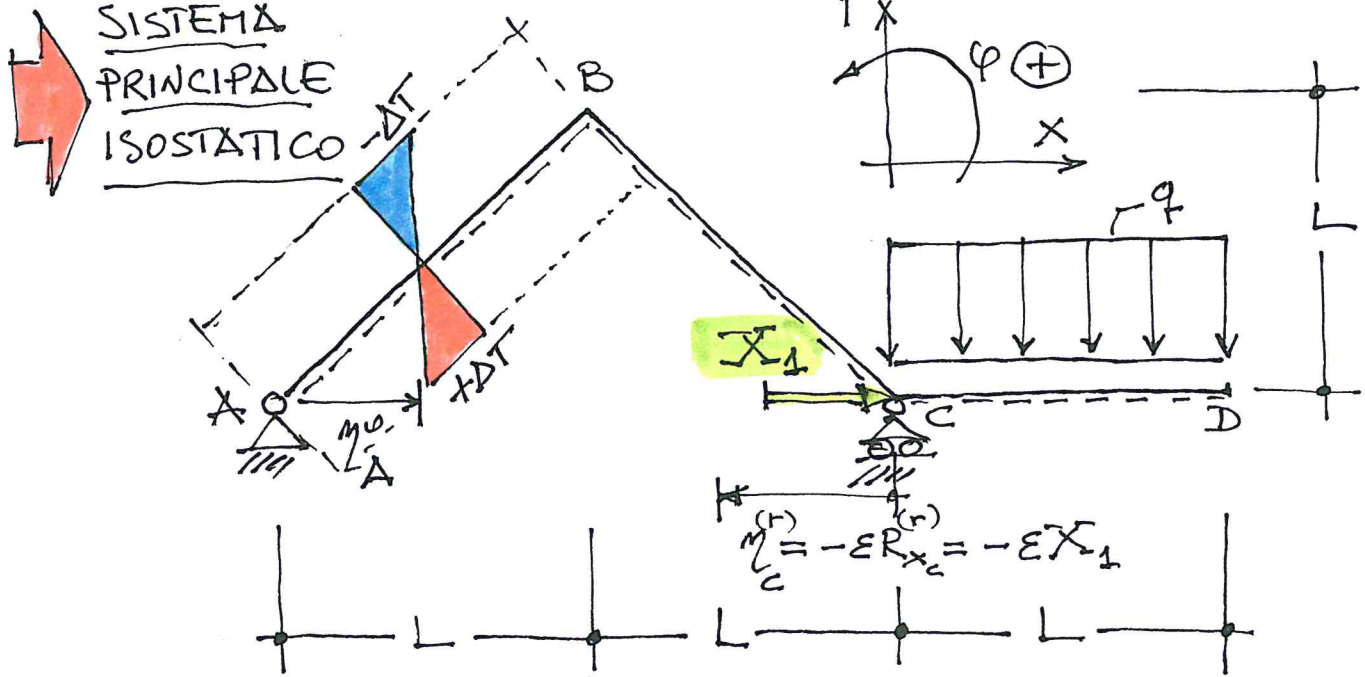
$$|\alpha\Delta T| = \frac{qL^2}{3EI}$$

➡ POSSIBILI SCELTE DEL SISTEMA PRINCIPALE ISOSTATICO:

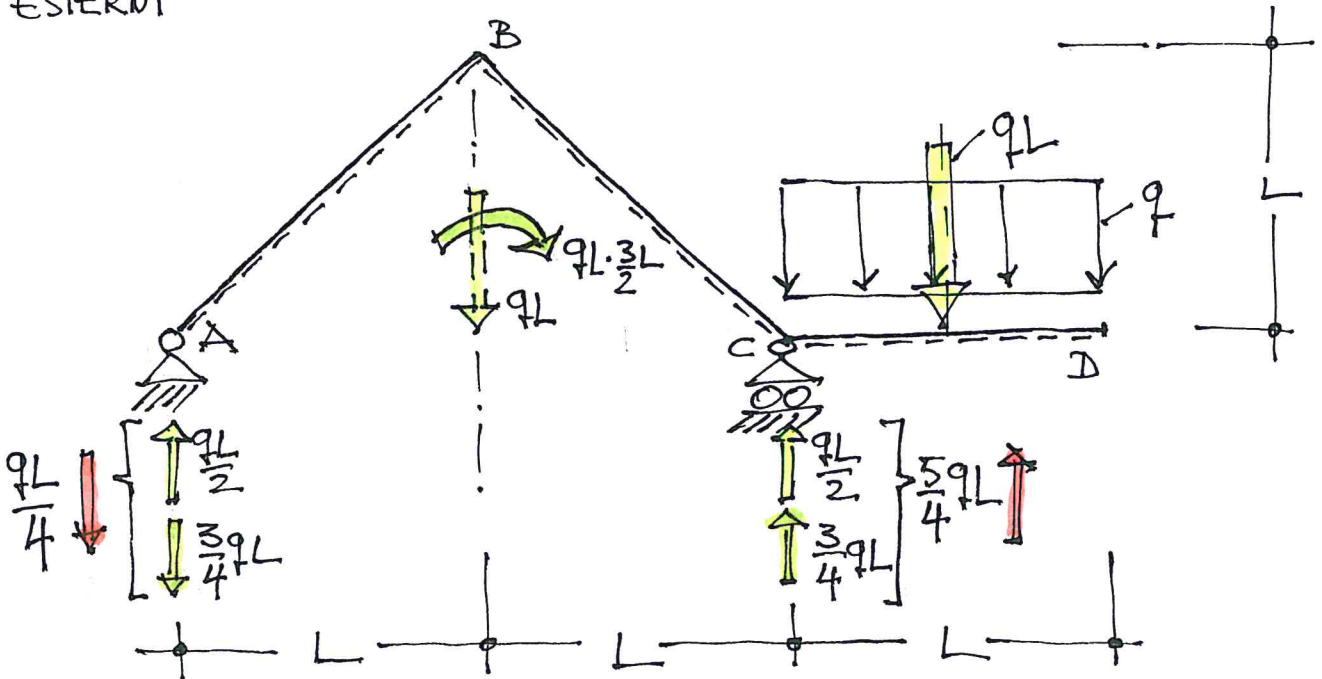


SOLUZIONE 1

II
FUSCHI
PISANO



SCHEMA [0]
SOLO CARICHI
ESTERNI

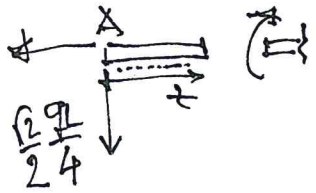


- I. Si calcolano le RV con metodo grafico!... vedi figura!... sposta qL !
- II. Si calcola $M^{(0)}(x)$ sui singoli tratti, si ha;

III

FUSCHI
PISANO

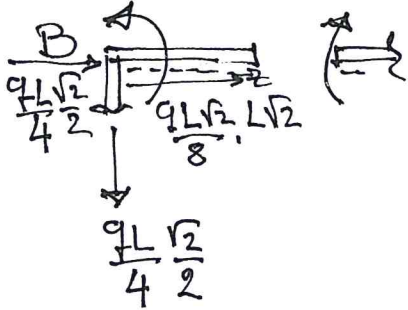
TRATTO AB $0 \leq z \leq L\sqrt{2}$



$$M^{(0)}(z) = -\frac{qL\sqrt{2}}{8}z$$

$$\begin{cases} M_A = 0 \\ M_B = -\frac{qL^2}{4} \end{cases}$$

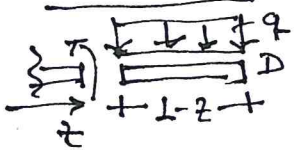
TRATTO BC $0 \leq z \leq L\sqrt{2}$



$$M^{(0)}(z) = -\frac{qL^2}{4} - \frac{qL\sqrt{2}}{8}z$$

$$\begin{cases} M_B = -\frac{qL^2}{4} \\ M_C = -\frac{qL^2}{4} - \frac{qL\sqrt{2}}{8} \cdot L\sqrt{2} = -\frac{qL^2}{4} - \frac{qL^2}{4} = -\frac{qL^2}{2} \end{cases}$$

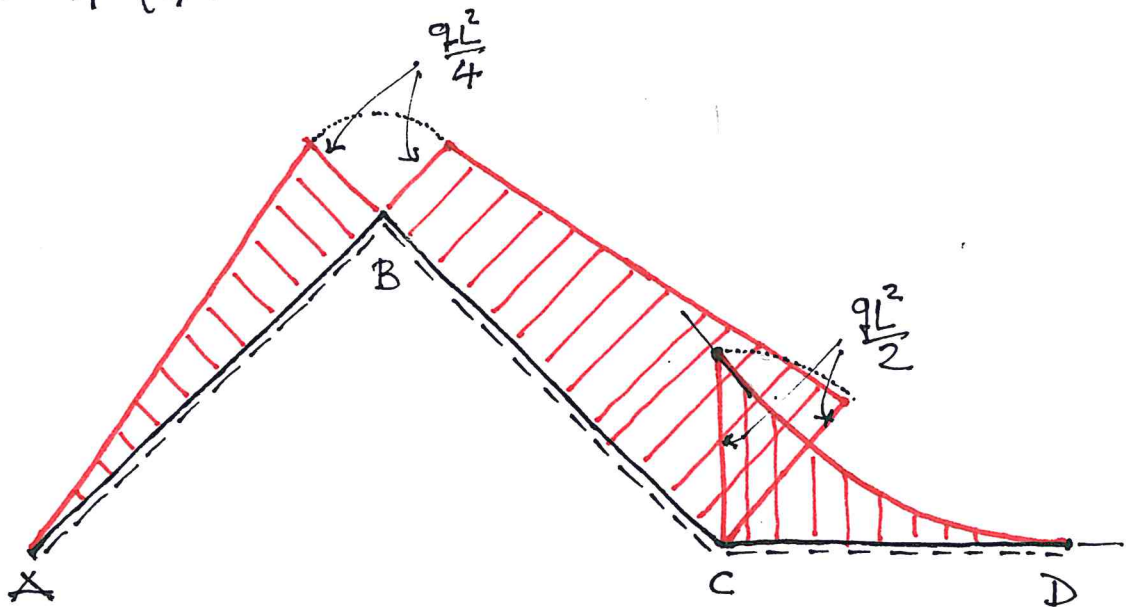
TRATTO CD $0 \leq z \leq L$




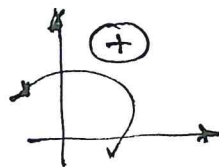
$$M^{(0)}(z) = -\frac{q(L-z)^2}{2}$$

$$\begin{cases} M_C = -\frac{qL^2}{2} \\ M_D = 0 \end{cases}$$

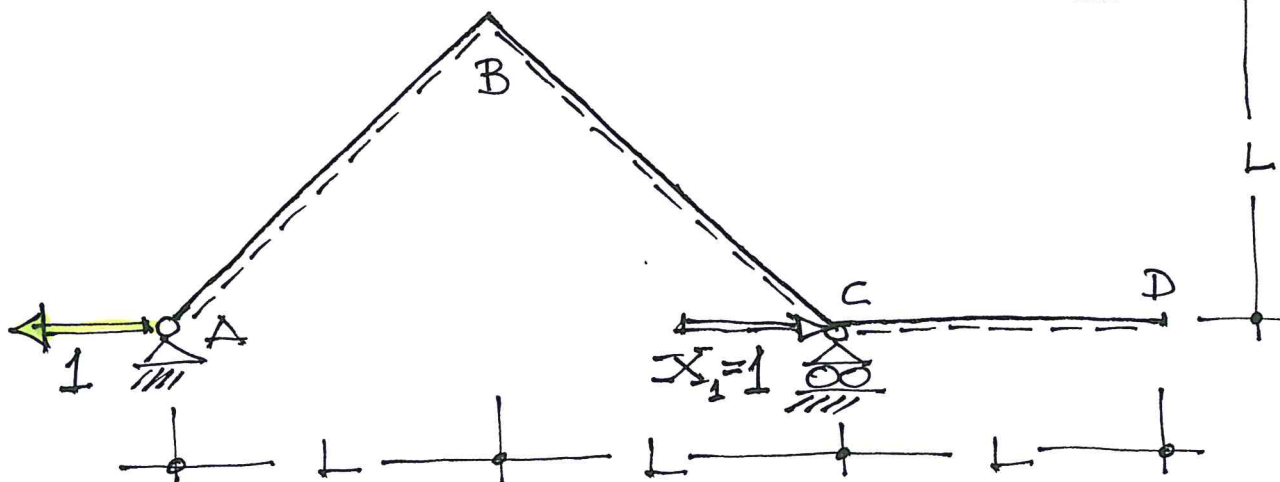
Diagramma $M^{(0)}(z)$:



 SCHEMA [1]
Solo $X_1 = 1$



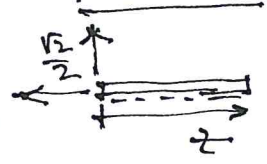
IV
FUSCHI
PISANO



I. Si calcolano le RN con metodo grafico! immediate!

II. Si calcola $M^{(1)}(z)$ sui singoli tratti, si ha:

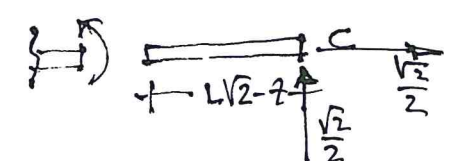
TRATTO AB $0 \leq z \leq L\sqrt{2}$



$$M^{(1)}(z) = \frac{\sqrt{2}}{2} z$$

$$\begin{cases} M_A = \phi \\ M_B = \frac{\sqrt{2}}{2} \cdot L\sqrt{2} = L \end{cases}$$


TRATTO BC $0 \leq z \leq L\sqrt{2}$

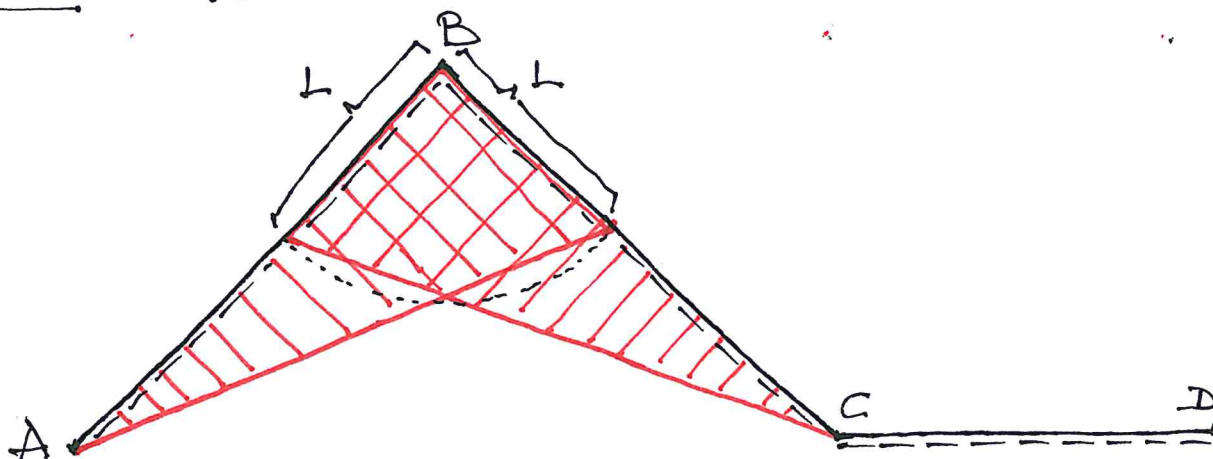


$$M^{(1)}(z) = \frac{\sqrt{2}}{2} [L\sqrt{2} - z]$$

$$\begin{cases} M_B = L \\ M_C = \phi \end{cases}$$

TRATTO CD $0 \leq z \leq L$ \rightarrow SCARICO !!

 DIAGRAMMA $M^{(1)}(z)$:





L'unica equazione di Müller-Breslau, corrispondente all'unica incognita iperstatica X_1 , si scrive nella forma $L_{ve} = L_{vi}$ assumendo come sistema lavorato o fittizio lo schema [1] e come sistema reale la struttura iperstatica data. Si ha:

(V)

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$$\begin{aligned}
 L_{ve} &= X_1^{(f)} \cdot \eta_i^{(r)} + \sum_j R_j^{(f)} \eta_j^{(r)} = \\
 &= 1 \cdot \underbrace{\eta_i^{(r)}}_{-\varepsilon X_1} + \underbrace{R_{X_A}^{(f)}}_{-1} \cdot \underbrace{\eta_A^0}_{\text{verso dx!}} = -\varepsilon X_1 - \eta_A^0
 \end{aligned}$$

$$L_{vi} = \int_{str} M^{(f)} \frac{M^{(r)}}{EI} dstr + \int_{str} M^{(f)} \frac{\alpha \Delta T}{h} dstr =$$

$\rightarrow \underbrace{M^{(f)} \equiv M^{(1)}} \quad \rightarrow \quad \underbrace{M^{(r)} = M^{(0)} + M^{(1)} X_1}$

$$= \int_{str} M^{(1)} \frac{M^{(0)}}{EI} dstr + X_1 \int_{str} \frac{[M^{(1)}]^2}{EI} dstr + \int_{str} M^{(1)} \frac{\alpha \Delta T}{h} dstr =$$

$$= \frac{1}{EI} \left\{ \int_{\overline{AB}} \left[\frac{\sqrt{2}}{2} z \right] \left[-\frac{9L\sqrt{2}}{8} z \right] dz + \int_{\overline{BC}} \left[\frac{\sqrt{2}}{2} [L\sqrt{2} - z] \right] \left[-\frac{9L^2}{4} - \frac{9L\sqrt{2}}{8} z \right] dz \right\} +$$

$$+ \frac{X_1}{EI} \left\{ \int_{\overline{AB}} \left[\frac{\sqrt{2}}{2} z \right]^2 dz + \int_{\overline{BC}} \left[\frac{\sqrt{2}}{2} (L\sqrt{2} - z) \right]^2 dz \right\}$$

$$+ \frac{\alpha \Delta T}{h} \int_{\overline{AB}} \frac{\sqrt{2}}{2} z dz =$$

$$= \frac{1}{EI} \left\{ \int_{\overline{AB}} -\frac{qL}{8} z^2 dz + \frac{\sqrt{2}}{2} \int_{\overline{BC}} \left\{ -\frac{qL^3\sqrt{2}}{4} - \cancel{\frac{qL^2}{8}z} + \cancel{\frac{qL^2}{4}z} + \frac{qL\sqrt{2}}{8}z^2 \right\} dz \right\} \text{FUSCHI PISANO} \quad \textcircled{\text{VI}}$$

$$+ \frac{X_1}{EI} \left\{ \int_{\overline{AB}} \frac{z^2}{2} dz + \frac{1}{2} \int_{\overline{BC}} (2L^2 + z^2 - 2L\sqrt{2}z) dz \right\} + \frac{\alpha \Delta T}{h} \int_{\overline{AB}} \frac{\sqrt{2}}{2} z dz =$$

$$= \frac{1}{EI} \left\{ -\frac{qL}{8} \int_0^{L\sqrt{2}} z^2 dz + \frac{\sqrt{2}}{2} \int_0^{L\sqrt{2}} \left[-\frac{qL^3\sqrt{2}}{4} + \frac{qL\sqrt{2}}{8} z^2 \right] dz \right\} +$$

$$+ \frac{X_1}{EI} \left\{ \int_0^{L\sqrt{2}} \frac{z^2}{2} dz + \frac{1}{2} \int_0^{L\sqrt{2}} [2L^2 + z^2 - 2L\sqrt{2}z] dz \right\} + \frac{\alpha \Delta T}{h} \int_0^{L\sqrt{2}} \frac{\sqrt{2}}{2} z dz =$$

$$= \frac{1}{EI} \left\{ -\frac{qL}{8} \left[\frac{z^3}{3} \right]_0^{L\sqrt{2}} + \frac{\sqrt{2}}{2} \left[-\frac{qL^3\sqrt{2}}{4} z + \frac{qL\sqrt{2}}{8} \left[\frac{z^3}{3} \right]_0^{L\sqrt{2}} \right] \right\} +$$

$$+ \frac{X_1}{EI} \left\{ \frac{1}{2} \left[\frac{z^3}{3} \right]_0^{L\sqrt{2}} + L^2 \left[z \right]_0^{L\sqrt{2}} + \frac{1}{2} \left[\frac{z^3}{3} \right]_0^{L\sqrt{2}} - L\sqrt{2} \left[\frac{z^2}{2} \right]_0^{L\sqrt{2}} \right\} + \frac{\alpha \Delta T \sqrt{2}}{2h} \left[\frac{z^2}{2} \right]_0^{L\sqrt{2}} =$$

$$= \frac{1}{EI} \left\{ -\cancel{\frac{qL^4}{12}\sqrt{2}} - \frac{qL^4}{4}\sqrt{2} + \cancel{\frac{qL^4}{12}\sqrt{2}} \right\} +$$

$$+ \frac{X_1}{EI} \left\{ \frac{L^3}{3}\sqrt{2} + \cancel{L^3\sqrt{2}} + \frac{L^3}{3}\sqrt{2} - \cancel{L^3\sqrt{2}} \right\} + \frac{\alpha \Delta T \sqrt{2}}{h} \frac{L^2}{2} =$$

$$= -\frac{qL^4}{4EI}\sqrt{2} + \frac{X_1}{EI} \frac{2}{3} L^3\sqrt{2} + \frac{\alpha \Delta T \sqrt{2}}{h} \frac{L^2}{2}$$

➡ In definitiva $L_{re} = L_{ri}$ fornisce:

$$-E X_1 - \eta_A^0 = -\frac{qL^4\sqrt{2}}{4EI} + \frac{X_1}{EI} \frac{2}{3} L^3\sqrt{2} + \frac{\alpha \Delta T}{h} \frac{\sqrt{2}}{2} L^2$$

quest'ultima, tenendo conto delle posizioni iniziali, si scrive:

$$-\frac{L^3\sqrt{2}}{3EI} X_1 - \frac{qL^4\sqrt{2}}{4EI} = -\frac{qL^4\sqrt{2}}{4EI} + \frac{X_1}{EI} \frac{2}{3} L^3\sqrt{2} + \frac{qL^2}{3EI} \cdot \frac{\sqrt{2}}{2} L^2$$

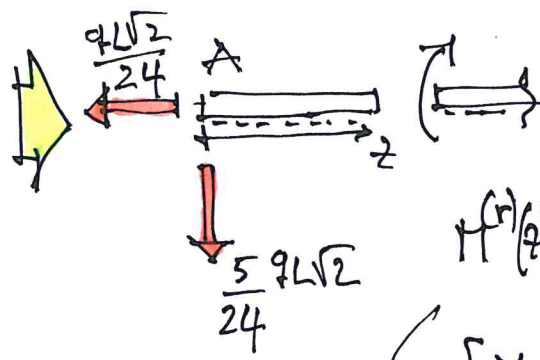
$$-L^3\sqrt{2} X_1 = \frac{qL^4\sqrt{2}}{6} \Rightarrow X_1 = -\frac{qL}{6} \Rightarrow \text{NEGATIVO!}$$

➡
Verso effettivo
opposto a quello
ipotesizzato!

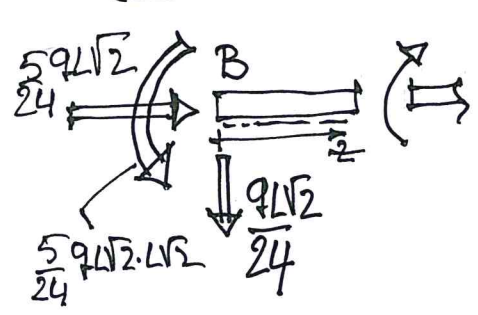


II. Si calcola $M^{(r)}(z)$ sui singoli tratti, si ha:

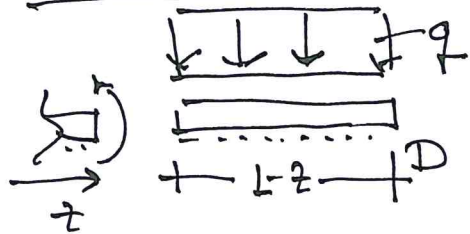
A diagram illustrating the decomposition of a force vector F into its horizontal component F_x and vertical component F_y . The force vector F is shown at an angle θ to the horizontal. The horizontal component is labeled $F_x = F \cos \theta$ and the vertical component is labeled $F_y = F \sin \theta$. The angle θ is also labeled as α in the diagram.



$$H'(z) = -\frac{59}{24} \sqrt{2} \cdot z$$

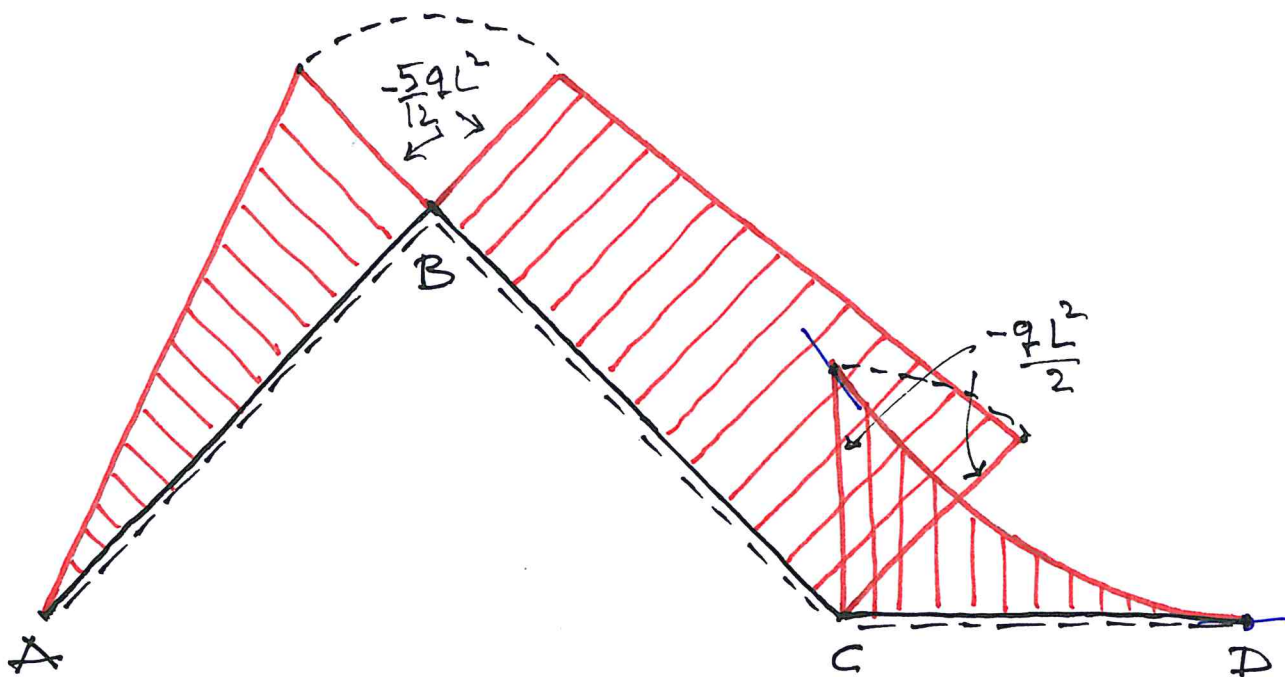
$$\hookrightarrow \begin{cases} \mu_A = \phi \\ \mu_B = -\frac{5}{12} q L^2 \end{cases}$$


$$M^{(w)}(z) = -\frac{5qL^2}{12} - \frac{qLz}{24} \quad \left\{ \begin{array}{l} M_B = -\frac{5qL^2}{12} \\ M_C = -\frac{qL^2}{2} \end{array} \right.$$

TRATTO CD $0 \leq z \leq L$ 

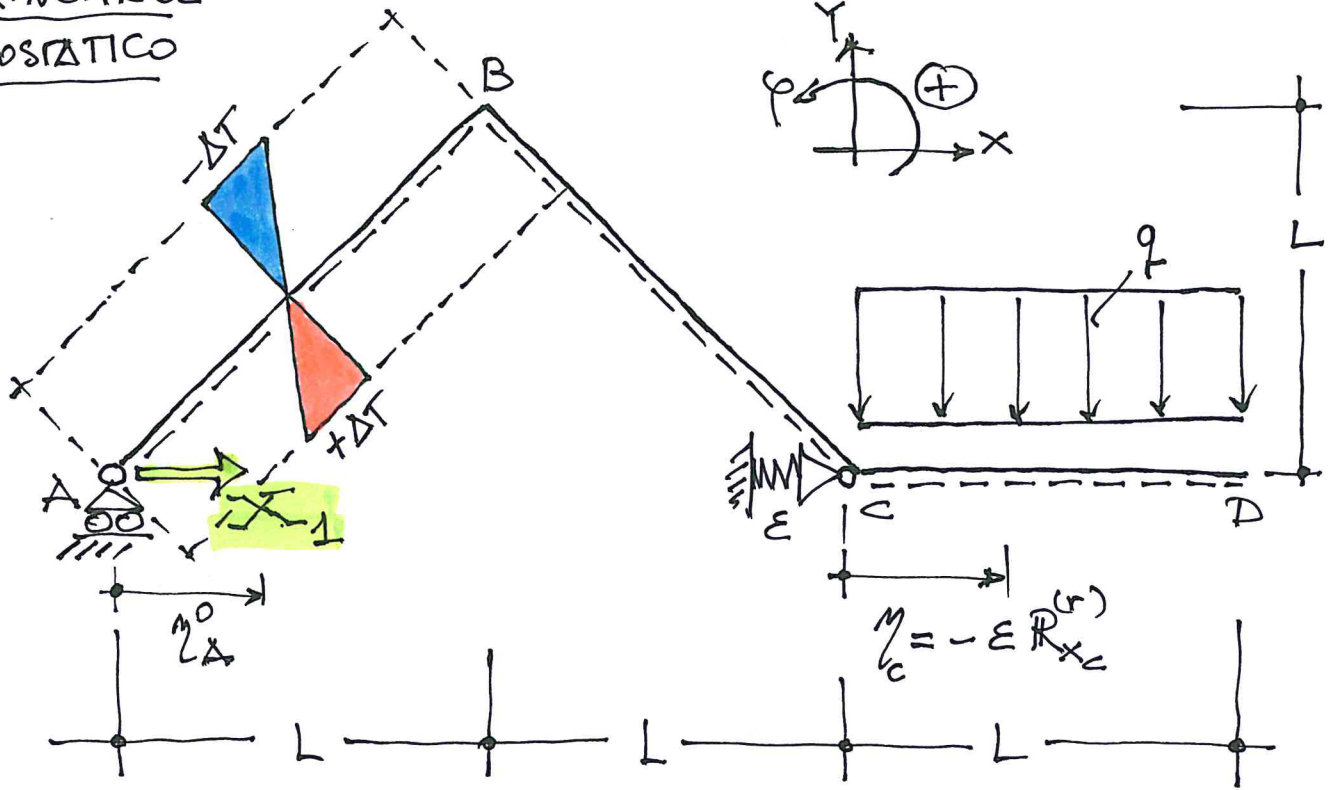
$$M^{(r)}(z) = -\frac{q(L-z)^2}{2}$$

$$\begin{cases} M_C = -\frac{qL^2}{2} \\ M_D = 0 \end{cases}$$

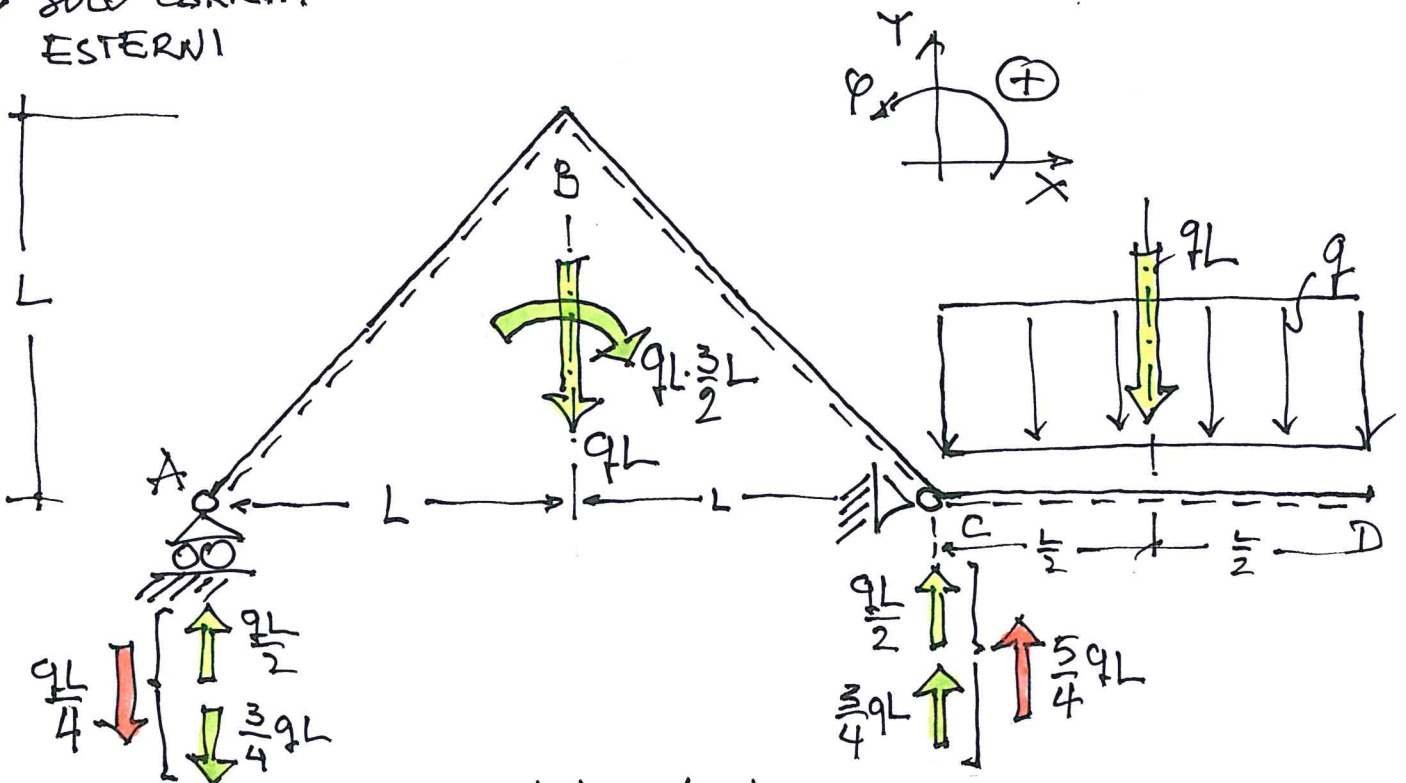
FUSCHI
PISANODIAGRAMMA FINALE $M^{(r)}(z)$ 

SOLUZIONE 2

**SISTEMA
PRINCIPALE
ISOSTATICO**



**SCHEMA [0]
SOLO CARICHI
ESTERNI**



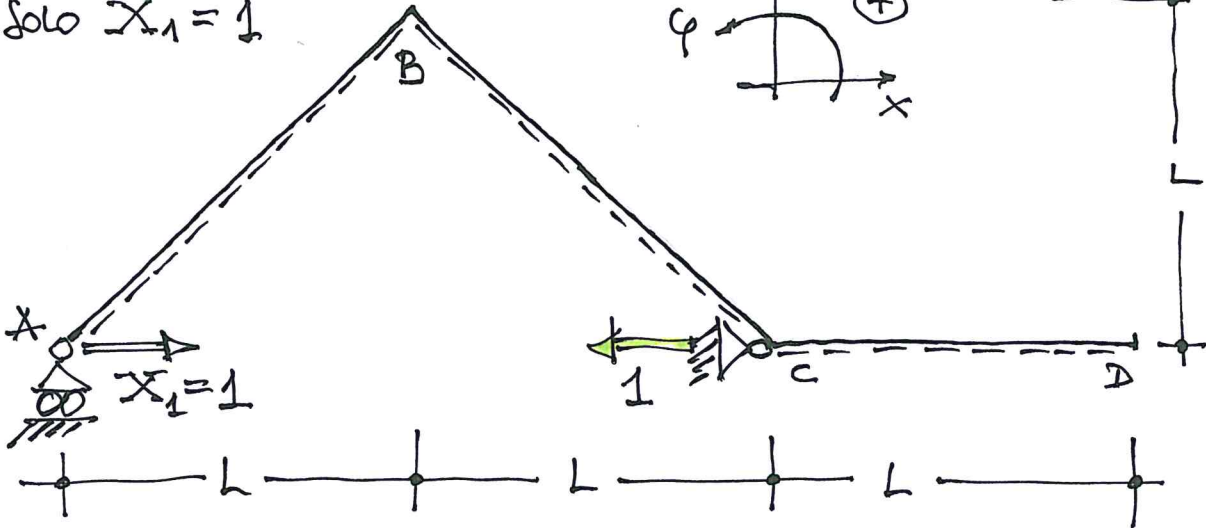
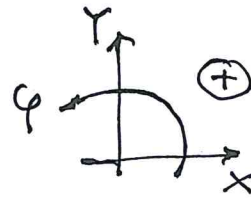
I. Si calcolano RV con metodo grafico!

II. Le leggi di $M^{(0)}(x)$ sono IDENTICHE a quelle della SOLUZ. n. 1 ∇ cfr. p. III



SCHEMA [1]

solo $X_1 = 1$



I. Si calcolano le RV con metodo grafico!... immediate!

II. Si calcola $M^{(1)}(z)$ sui singoli tratti, si ha:

TRATTO AB $0 \leq z \leq L\sqrt{2}$

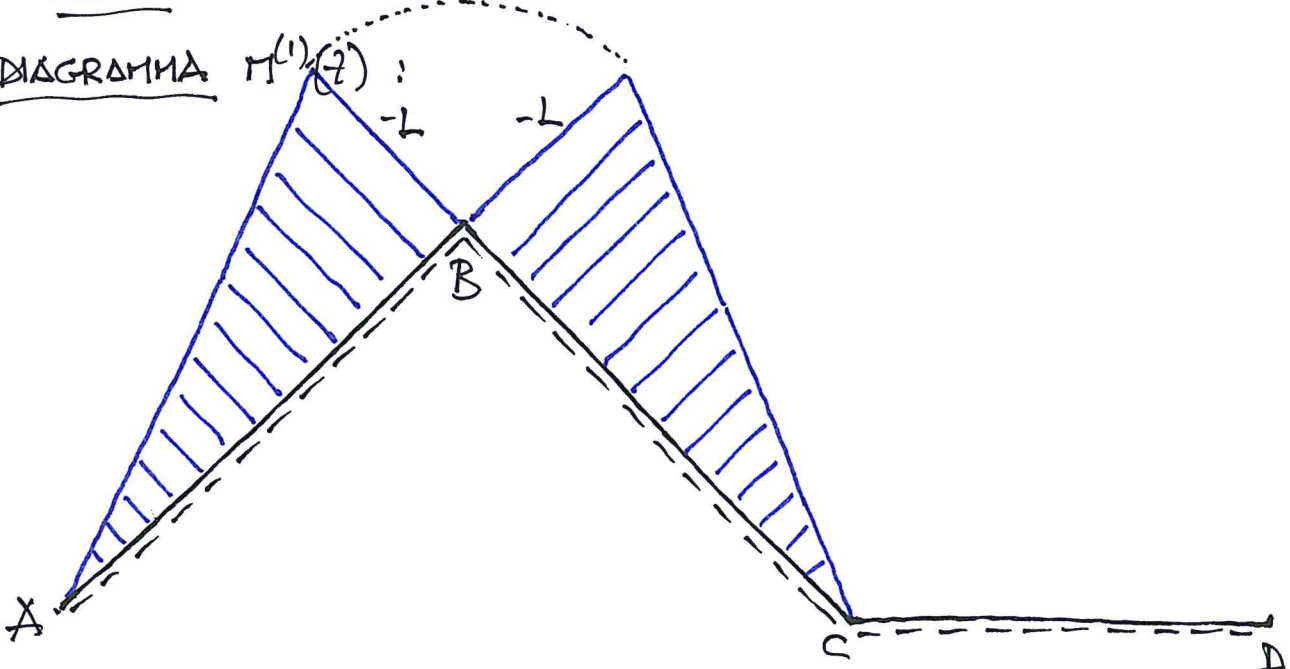
$$\begin{aligned} & \text{Diagramma di forze interne su AB: } \left[M^{(1)}(z) = -\frac{\sqrt{2}}{2} z \right] \\ & \left\{ \begin{array}{l} M_A = \phi \\ M_B = -\frac{\sqrt{2}}{2} \cdot L\sqrt{2} = -L \end{array} \right. \end{aligned}$$

TRATTO BC $0 \leq z \leq L\sqrt{2}$

$$\begin{aligned} & \text{Diagramma di forze interne su BC: } \left[M^{(1)}(z) = -\frac{\sqrt{2}}{2} [L\sqrt{2} - z] \right] \\ & \left\{ \begin{array}{l} M_B = -L \\ M_C = \phi \end{array} \right. \end{aligned}$$

TRATTO CD \rightarrow scarico!

DIAGRAMMA $M^{(1)}(z)$:



13. Confrontando l'ultima espressione con quella analoga della soluzione n. 1 (2 pag. V) si osserva che il primo addendo (con termine $\frac{1}{EI}$ in evidenza) è uguale a quello già sviluppato per la solut. 1 cambiato di segno; il secondo addendo (con $\frac{X_1}{EI}$) è identico a quello visto in precedenza in quanto le leggi di $M^{(1)}$, pur essendo negative in questo caso sono da considerarsi al quadrato; il terzo addendo infine è di nuovo pari a quello di pag. V cambiato di segno!

Risulta quindi (cfr. p. VI):

$$L_{vi} = \frac{qL^4}{4EI} \sqrt{2} + \frac{X_1}{EI} \frac{2L^3}{3} \sqrt{2} - \frac{\alpha \Delta T}{h} \frac{\sqrt{2}}{2} L^2$$

In definitiva $L_{re} = L_{vi}$ fornisce in questo caso:

$$M_A^0 - E X_1 = \frac{qL^4}{4EI} \sqrt{2} + \frac{X_1}{EI} \frac{2L^3}{3} \sqrt{2} - \frac{\alpha \Delta T}{h} \frac{\sqrt{2}}{2} L^2$$

Tenendo conto delle posizioni iniziali e semplificando si ha:

$$\cancel{\frac{qL^4}{4EI} \sqrt{2}} - \cancel{\frac{L^3}{3EI} X_1} = \cancel{\frac{qL^4}{4EI} \sqrt{2}} + \frac{X_1}{EI} \frac{2L^3}{3} \sqrt{2} - \cancel{\frac{\alpha \Delta T}{h} \frac{\sqrt{2}}{2} L^2}$$

$$\frac{L^3}{EI} X_1 = \frac{qL^2}{3EI} \frac{L^2}{2} \Rightarrow X_1 = \frac{qL}{6} \text{ positiva!}$$

OK! cfr. p. VII
con le R.V.
ottenute a partire
dalla solut. 1!